

# Current Biology

## Collective Force Regulation in Anti-parallel Microtubule Gliding by Dimeric Kif15 Kinesin Motors

### Highlights

- Kif15 transports microtubules in bundles through motor and non-motor coordination
- Kif15's non-motor microtubule-binding site (Coil-1) is stronger than stall force
- Kif15 generates force in anti-parallel bundles and has a force-feedback mechanism
- Coil-1 tethering is needed for the force ramp and plateau in anti-parallel bundles

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### In Brief

Reinemann et al. investigate the mechanical properties and force generation capabilities of the mitotic kinesin Kif15 using optical tweezers. Measurements of motor subdomains, single motors, and motor-microtubule bundles paired with stochastic simulations reveal a mechanism for how Kif15 can rescue bipolar spindle assembly upon Eg5 inhibition.



# Collective Force Regulation in Anti-parallel Microtubule Gliding by Dimeric Kif15 Kinesin Motors

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## SUMMARY

During cell division, the mitotic kinesin-5 Eg5 generates most of the force required to separate centrosomes during spindle assembly. However, Kif15, another mitotic kinesin, can replace Eg5 function, permitting mammalian cells to acquire resistance to Eg5 poisons. Unlike Eg5, the mechanism by which Kif15 generates centrosome separation forces is unknown. Here we investigated the mechanical properties and force generation capacity of Kif15 at the single-molecule level using optical tweezers. We found that the non-motor microtubule-binding tail domain interacts with the microtubule's E-hook tail with a rupture force higher than the stall force of the motor. This allows Kif15 dimers to productively and efficiently generate forces that could potentially slide microtubules apart. Using an in vitro optical trapping and fluorescence assay, we found that Kif15 slides anti-parallel microtubules apart with gradual force buildup while parallel microtubule bundles remain stationary with a small amount of antagonizing force generated. A stochastic simulation shows the essential role of Kif15's tail domain for load storage within the Kif15-microtubule system. These results suggest a mechanism for how Kif15 rescues bipolar spindle assembly.

## INTRODUCTION

A hallmark of the G2/M transition is the conversion of an interphase microtubule cytoskeleton into a bipolar spindle. Bipolarity is essential for spindle function and is established by many microtubule-associated proteins that collectively move centrosomes to opposite cell poles [1]. One factor central to spindle assembly is the homotetrameric kinesin-5, Eg5, that

crosslinks and slides anti-parallel microtubules apart [2]. Eg5 inactivation blocks centrosome separation, resulting in a monopolar spindle [3–10]. However, several lines of evidence indicate that kinesin-12s also generate forces relevant for spindle assembly. In *C. elegans*, a kinesin-12 (KLP-18) rather than kinesin-5 (BMK-1) is essential for spindle formation [11, 12]. In humans, kinesin-12 Kif15 prevents [13] or slows [14] kinesin-5 inhibitor (K5I)-triggered collapse of the metaphase spindle. Kif15 overexpression can nullify the cytotoxic effects of K5Is by driving spindle assembly [13, 15] and is essential for HeLa cells to acquire K5I resistance [16]. These results suggest that kinesin-5s and kinesin-12s share strong functional homology, but the biophysical underpinnings are unclear because the motors differ in their cell biological and biochemical properties.

In mammalian cells, the mitotic localizations of Kif15 and Eg5 are significantly different. Kif15 enriches on kinetochore microtubules in prometaphase and then distributes uniformly along spindle microtubules at metaphase [17]. In contrast, Eg5 binds microtubules early during spindle assembly irrespective of whether they are attached to kinetochores [3, 17] and concentrates near spindle poles at metaphase [3, 10, 18]. In K5I-resistant cell lines (KIRCs), Kif15 redistributes to non-kinetochore microtubules while microtubule-bound levels of active Eg5 are reduced [16, 17]. These localization patterns may indicate that Kif15 can only produce forces sufficient to drive spindle assembly when it is bound to non-kinetochore microtubules in an orientation-dependent manner. Kinetochore microtubules are predominantly parallel oriented [19], whereas inter-polar microtubules are of mixed polarity [20]. Redistribution of Kif15 to non-kinetochore microtubules may lead to significant force production when microtubules are anti-parallel, similar to Eg5.

Elegant biophysical studies have demonstrated that tetrameric Eg5 is optimally designed to drive spindle assembly [2, 21–25]. Eg5 only slides anti-parallel microtubules apart [2]. Single-molecule and stopped-flow experiments have shown that Eg5 resides primarily in a two-head bound state [21], and its catalytic cycle is limited by ATP hydrolysis rather than product release [22]. These features and a second non-motor

microtubule-binding site bias Eg5 to remain attached to microtubules [24]. Furthermore, Eg5's mechanochemical cycle makes force generation scale linearly with motor number within an anti-parallel microtubule overlap [25].

By comparison, our understanding of Kif15 is limited. Some work suggests that Kif15 is tetrameric [26], leading to speculation that Kif15 promotes spindle assembly through a mechanism similar to Eg5, while our previous studies indicate that Kif15 is dimeric [16, 27]. As a homodimer, Kif15 can crosslink two microtubules through its motor domains and a second microtubule-binding site (Coil-1) within its coiled-coil stalk [27]. This crosslinking activity enables Kif15 to slide microtubules apart *in vitro* [27], although the microtubule orientation requirement for this activity is unknown.

Here, we investigate the activity of Kif15 on single microtubules and within microtubule bundles of different filament arrangements. We analyze constructs including full Kif15, a truncated Kif15 motor that does not include the Coil-2 inhibitory domain but includes the non-motor microtubule-binding domain Coil-1 (N700), and the isolated microtubule-binding domain (Coil-1) (Figure 1A). Single-molecule optical tweezers and fluorescence experiments confirm that Kif15 acts as a dimer, takes a large percentage of backward steps, and that Coil-1 sustains forces higher than motor stall. These properties permit buildup of mechanical strain in the microtubule system through forward progress of the motor heads and concomitant resistance or relaxation by Coil-1 rupturing and backstepping. We further show that concerted movement occurs exclusively in anti-parallel microtubules. A stochastic simulation of microtubule sliding by Kif15 reveals the mechanism by which Coil-1 regulates strain buildup. Our work provides insight into how Kif15 generates forces that drive spindle assembly and has implications for the interplay between Eg5 and Kif15 within the spindle.

## RESULTS

### Oligomerization State of Kif15

We used the baculovirus expression system to produce and purify Kif15 motor constructs (Kif15 and N700) with a C-terminal GFP-His6-tag (Figure 1B, inset) [27]. Confirmation of the motor's oligomerization state was necessary to form the foundation of a mechanism regarding Kif15's ability to generate force during spindle assembly. Single-molecule photobleaching of individual motors occurred in two steps (STAR Methods; Figures S1A–S1C). This indicates that our construct is a dimer, which agrees with previous rigorous analysis in solution and when expressed in cells [16, 27, 28].

### N700 Generates Force at the Single-Molecule Level

To evaluate the force generation capabilities of Kif15 and N700, single-molecule bead motility assays using optical tweezers were performed (Figure 1B; STAR Methods) [29]. N700, which includes the motor, stalk, and Coil-1 [27], moved robustly, permitting evaluation of motor characteristics such as stall force, step size, backward step probability, and dwell times. Full-length Kif15, containing a C-terminal inhibitory domain (Coil-2) [27], moved much less frequently, prompting rigorous analysis of N700.

N700 exhibited a higher frequency of motility events compared to kinesin-1, and traces did not reach a plateauing

stall but rather fell off abruptly, similar to sawtooth patterns generated by Eg5 [23]. Its stall force was  $3.0 \pm 0.6$  pN (average  $\pm$  SD,  $n = 102$ ; Figure 1C), which is similar to that of Kif15 (see below). N700 took approximately 8-nm steps (size of a tubulin dimer), though some variability was observed (Figure 1D). Backward stepping was observed with a 32% frequency, well above that of kinesin-1 [29–31]. While the vast majority of step sizes were 8 nm, a small population (20%) of 16-nm forward steps was recorded (blue and green constrained fits in Figure 1D), which were likely to be unresolvable rapid 8-nm steps in succession. N700 had 2.7-s dwell times (Figure 1E).

N700 (attached to a bead) moved readily in an unloaded motility assay. Its velocity was  $75.8 \pm 41$  nm s<sup>-1</sup> ( $n = 67$ ; Figure 1F), which is similar to previous measurements of Eg5 [23] and fluorescence velocity measurements of N700 and Kif15 [26, 27]. The average run length was  $5,120 \pm 2,900$  nm ( $n = 67$ ; Figure 1G). The spread was due to the underlying microtubule length, and values up to 12  $\mu$ m were measured. Long commitments of Kif15 to motility have been observed previously [26, 27]. Upon reaching the end of the microtubule, N700 released 64% of the time. It also had the ability to switch microtubule tracks (Movie S1), as shown previously, but the proposed structure was a tetramer [26]. Instead, N700 can switch tracks likely via its ability to rapidly recommit to motility, as shown by its high run frequency, along with Coil-1 that facilitates attachment and can keep an unbound motor from diffusing away (see below).

### Force-Velocity Analysis of N700

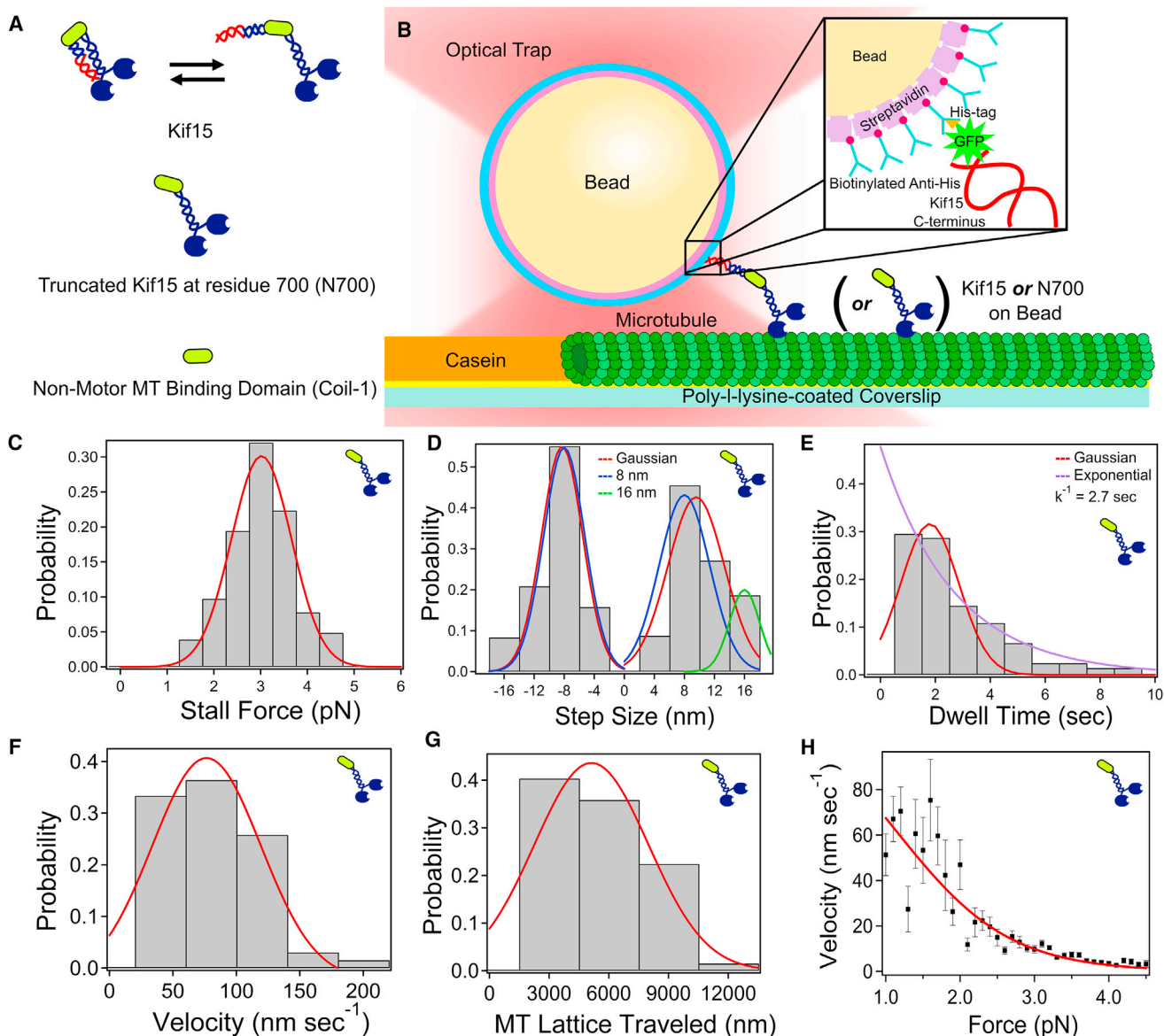
To parameterize the mechanistic underpinnings of Kif15 behavior, a force-velocity curve was generated for N700 (Figure 1H; STAR Methods) [32–34], and was fit with a three-state kinetic model of the form [23, 34]

$$v(F) = \frac{\delta_1 k_1 k_2 k_3 [ATP]}{k_1 (k_2 + k_3) [ATP] + k_3 (k_2 + k_{-1})} \quad (\text{Equation 1})$$

with the force-dependent rate of the mechanochemical cycle

$$k_2 = k_2^0 e^{-\delta_2 F / k_B T}. \quad (\text{Equation 2})$$

Here,  $v$  is the motor velocity under an applied force  $F$ ;  $\delta_1 = 8.2$  nm is the average kinesin step size;  $k_1$  and  $k_{-1}$  are ATP binding and unbinding rates (globally fit from [23]);  $k_2^0$  is the unloaded mechanical rate;  $k_3$  is the ATP hydrolysis rate;  $k_B T$  ( $T = 300$  K) is thermal energy; and  $\delta_2$  represents the force sensitivity of the three-state model, where larger values indicate a more force-sensitive motor [34]. The measured and fitted parameters for kinesin-1 [34], Eg5 [23], N700, and Kif15 are shown in Table 1, where  $\delta_1$ ,  $k_1$ , and  $k_{-1}$  were held constant. Eg5 and N700 unloaded velocities are similar, but N700 is more processive than Eg5, potentially due to the N700's ability to recommit to motility upon unbinding from the microtubule. The force sensitivity  $\delta_2$  is smaller for Eg5 (1.9 nm) than kinesin-1, N700, and Kif15 (4–6 nm). Eg5 has a proline in the middle of the neck linker, resulting in a shorter cover-neck bundle (force-generating element) compared to kinesin-1 or Kif15, agreeing with its shorter  $\delta_2$  [34]. These parameters dictate Kif15's single-molecule- and ensemble-level force generation capacity (see modeling results).



**Figure 1. N700 Motility Assay**

(A) Constructs studied: Kif15, N700, and Coil-1.

(B) Single-molecule motility assay (STAR Methods).

(C) N700 stall force, averaging  $3.0 \pm 0.6$  pN ( $n = 102$ ), which is very similar to Kif15.

(D) Step size distribution, averaging  $9.6 \pm 3.8$  nm ( $n = 473$ , forward) and  $8.3 \pm 2.7$  nm ( $n = 230$ , backward). Blue and green, 8- and 16-nm constrained fits.

(E) Dwell time between steps averaged  $1.8 \pm 1.1$  s. Decay constant (exponential fit, red) is 2.7 s.

(F) Unloaded velocity measured via video tracking was found to be  $75.8 \pm 41$  nm s<sup>-1</sup> ( $n = 67$ ).

(G) N700 processivity was measured via video tracking the run length as  $5,120 \pm 2,900$  nm, which is limited by microtubule length ( $n = 67$ ).

(H) Force-velocity curve. Solid line, fit with a three-state kinetic model (Table 1). Error bars, SEM.

See also Figure S1 and Movie S1.

### Kif15 and N700 Stall at 3 pN

Interestingly, Kif15 was much slower than N700 and had a lower run frequency, or number of run events (walk until maximum force was reached before returning to the trap center) per time, on average 1.2 and 10 runs per 100 s for Kif15 and N700, respectively (based on run events from raw force/displacement data). This suggests that Coil-2 in Kif15 plays a regulatory role, a feature not fully replicated in the trapped bead assay. Kif15

also showed step size variability in the distribution but showed 8-nm steps near the stall force (Figure 2). Kif15's stall force was very similar to N700 (Figure 2C). Step size distributions (Figure 2D) also contained 8-nm (blue) and 16-nm (green; 10% of forward and 20% of backward steps) constrained fits.

Unlike N700, Kif15 unloaded motility on single microtubules was rare. Although Kif15-coated beads bound microtubules, they did not readily move, making it difficult to obtain unloaded

**Table 1. Three-State Kinetic Model**

Construct	Unloaded Velocity (nm s <sup>-1</sup> )	Run Length (nm)	Stall Force (pN)	Three-State Model					
				$k_1$ (μM <sup>-1</sup> s <sup>-1</sup> )	$k_{-1}$ (s <sup>-1</sup> )	$k_2^0$ (s <sup>-1</sup> )	$k_3$ (s <sup>-1</sup> )	$\delta_2$ (nm)	$v_{\max}$ (nm s <sup>-1</sup> )
Kinesin-1 [34]	671 ± 21	1,370 ± 287	4.92 ± 0.08	2	120	12,900	76.86	5.50	630
Eg5 [23, 34]	96 ± 2	67 ± 7	1.5–7 <sup>a</sup>	0.89	10	86	13.5	1.9	94
N700	76 ± 41	5,120 ± 2,900	3.0 ± 0.6	2	120	72.2	15.1	5.4	101
Kif15	n/m	n/m	2.7 ± 1.0	2	120	88.1	16.2	4.1	111

Kinesin-1 and Eg5 values were added for comparison. n/m, not measured.

<sup>a</sup>Range of values reported.

measurements. This may be because both Coil-1 and the motor domains bound to the microtubule simultaneously, making motility dependent on whether the motor heads could produce enough force to displace Coil-1 (see below). When motile, traces resembled those of N700 and Eg5. Notably, Kif15 moved processively even with the inhibitory Coil-2 domain present (Movie S2). This could be an effect of the GFP tag or close association of the C terminus to the bead, both of which could sequester Coil-2 from association with the motor heads.

### Coil-1 Resists Forces Greater Than Stall

We investigated the Coil-1/microtubule interaction, which would be critical in defining motor function. A Coil-1 rupture force below the stall force implies that motor heads walking along a microtubule would easily rupture Coil-1 bound to an adjacent microtubule, facilitating isolated motor movement with little resistance. A rupture force higher than stall would anchor Coil-1 to the microtubule while the crosslinked motor heads walk along the other, permitting productive, efficient, and collective force buildup within the bundle and concomitant microtubule transport.

We evaluated the strength of the Coil-1/microtubule interaction by measuring the time for the bond to rupture at a load determined by the necessary displacement to fully elongate the DNA tether (Figure 3; STAR Methods). The lifetime distribution was bimodal, which averaged  $5.6 \pm 1.6$  s and  $24.8 \pm 7.9$  s, respectively ( $n = 109$ ; Figure 3B). This potentially reflects binding of Coil-1 to the microtubule's C-terminal tail (termed E-hook) or to the microtubule lattice. In both cases, the rupture forces were higher than the 3-pN stall force (Figure 3C). The average lifetime was long relative to the dwell times measured for Kif15, suggesting that Kif15 may be able to generate force in microtubule bundles. Interestingly, a significant number of rupture traces showed structured motion toward the trap center before rupture (Figure 3G, blue; Figure S2). The transitions appeared discrete with dwells in between (Figure S2, insets). This structure suggests that Coil-1 may jump to the next available E-hook to re-adjust its position and maintain the high level of resistance necessary for force generation.

We further investigated the role of the negatively charged E-hook by cleaving it from microtubules with subtilisin. Digested microtubules were confirmed by fractionation of  $\alpha$ - and  $\beta$ -tubulin bands in SDS-PAGE (Figure 3D) [35]. Rupture measurements with digested microtubules revealed a reduced lifetime ( $5.2 \pm 1.4$  s,  $n = 49$ ; Figure 3E) and rupture force ( $3.4 \pm 1.4$  pN,  $n = 49$ ; Figure 3F). The rupture trace on a digested microtubule (Figure 3G, red) was also noticeably flat compared to normal mi-

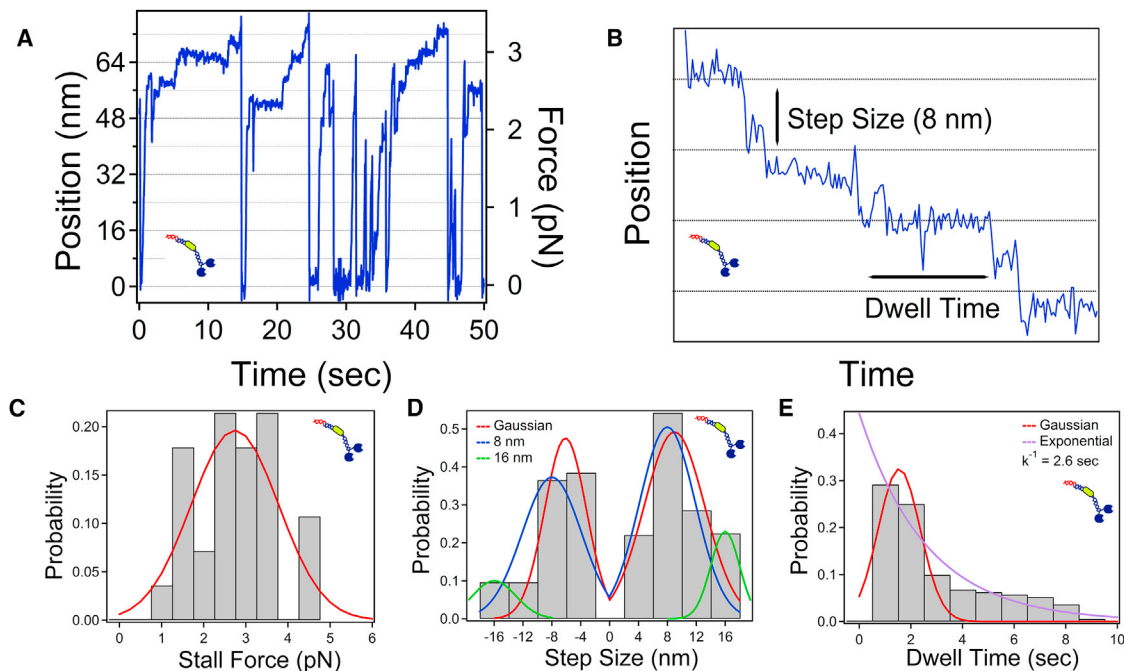
cro-tubules (Figure 3G, blue). The difference may be due to the lack of available E-hooks to rescue binding once the first binding event fails. The marked lifetime decrease under a given rupture force (Figure 3H) also supports that the E-hook plays a substantial, most likely electrostatic, role in binding Coil-1 to microtubules. The dependence on lifetime for Coil-1 on microtubules and digested microtubules was fit to an exponential based on the Bell model [36], which describes the force dependence of bond reaction rates (Figure 3H). Coil-1 lifetime on digested microtubules fell off quickly with increased force in contrast to the relatively flat dependence for native microtubules, revealing the E-hook's significance in the interaction.

Under physiological conditions, Kif15 targets kinetochore microtubules that contain parallel microtubules [17]. However, in KIRCs, Kif15 also binds inter-polar microtubules that are oriented in anti-parallel [16, 17]. Thus, Kif15 may somehow discriminate and perform differently between bundle orientations. For example, if Kif15, being a plus-end-directed motor, can slide anti-parallel microtubules apart, then the Coil-1/microtubule interaction should be strong enough to sustain load as the motor walks. Conversely, if Kif15 transits through parallel bundles, then a weaker Coil-1/microtubule interaction would be advantageous in facilitating motor transport toward the plus end.

To test Coil-1's orientation-sensing ability, a directional pulling assay was performed, similar to the assay in Figure 3A, except using polarity-marked microtubules (STAR Methods) [37]. After the tether was formed in differential interference contrast (DIC) mode, fluorescence visualization unambiguously determined the microtubule orientation. The piezostage was then moved toward the desired microtubule end and the system was held at a fixed force. The average rupture forces for pulling toward the plus end ( $7.7 \pm 2.6$  pN,  $n = 26$ ) and the minus end ( $7.8 \pm 3.8$  pN,  $n = 30$ ) were similar, most likely due to the E-hook's flexibility and reorientation ability. Thus, Coil-1 should respond similarly when Kif15s walk between microtubules in parallel or anti-parallel.

### Kif15 Generates Force in Anti-parallel Microtubule Bundles

An in vitro optical trapping assay was developed to observe Kif15 behavior in microtubule bundles, a more native environment compared to the bead assay (Figure 4A; STAR Methods, adopted from Shimamoto et al. [25]). After finding a bundle, its orientation (parallel versus anti-parallel) was determined through fluorescence visualization relative to the known fixed trap position. Since the streptavidin bead only binds the biotinylated



**Figure 2. Kif15 Motility Assay**

(A) Example Kif15 motility trace.

(B) Example of 8-nm stepping used for step size and dwell time analysis.

(C) Stall force histogram, averaging  $2.7 \pm 1.0$  pN ( $n = 27$ ).

(D) Step size, averaging  $8.9 \pm 4.1$  nm ( $n = 118$ , forward) and  $6.1 \pm 2.9$  nm ( $n = 52$ , backward). 8-nm (blue) and 16-nm (green) constrained fits are shown.

(E) Dwell time, averaging  $1.5 \pm 0.8$  s. Decay constant (exponential fit, purple) is 2.6 s.

See also [Movie S2](#).

tubulin contained in the minus end microtubule seed, the trap center is located at the cargo microtubule minus end ([Figure 4B](#)).

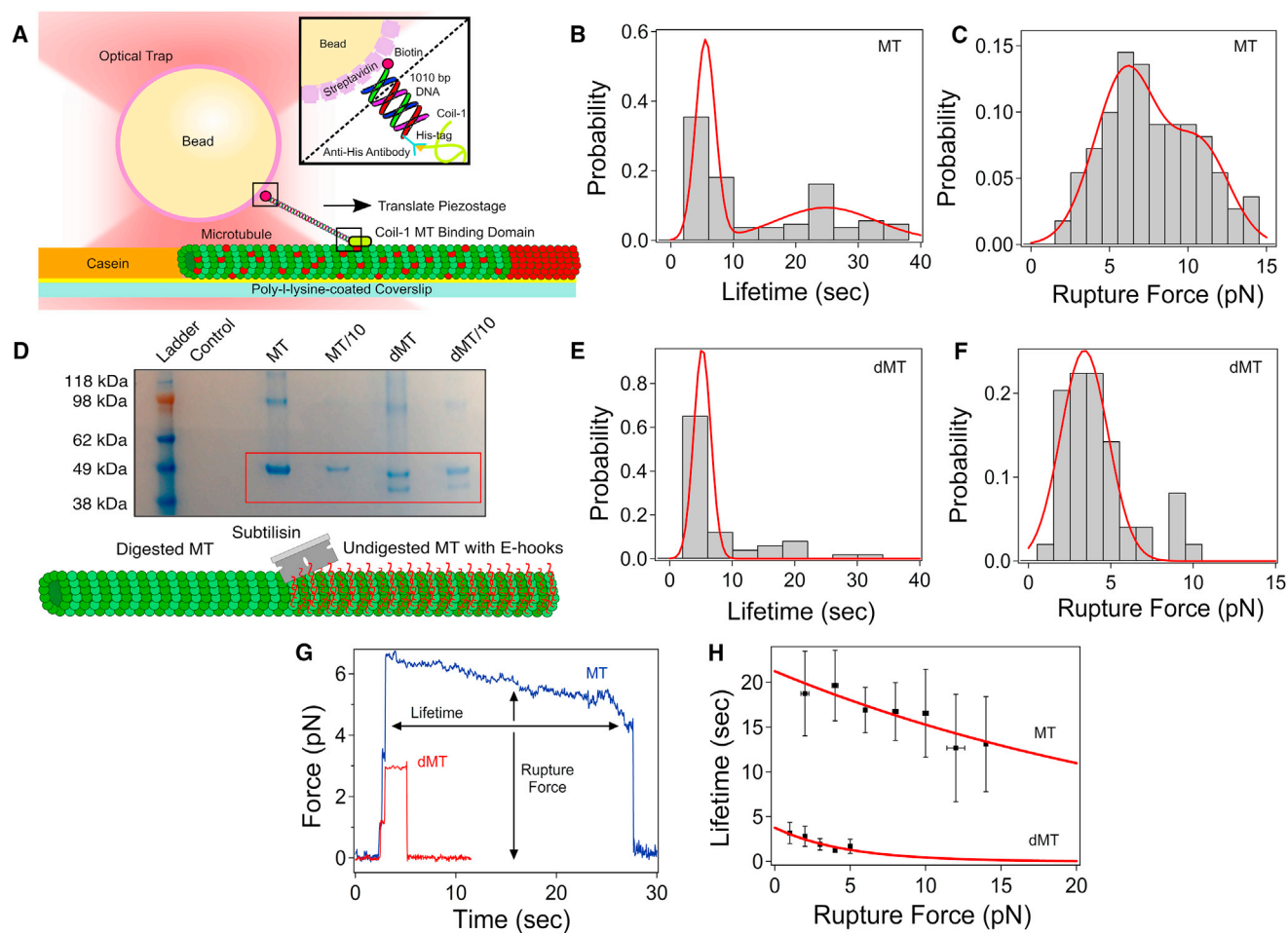
Bundles were generated in the presence of  $\sim 20$  nM Kif15. Parallel bundle traces did not show much force generation but rather exhibited wandering along the baseline with motors antagonizing each other ( $n = 43$ ; [Figure 4C](#)). To determine whether this baseline displacement was due to the motors or thermal fluctuations, a control was performed with AMPPNP that locks the motors in place. The trace with ATP present shows distinctive motion in comparison to the AMPPNP trace, revealing that this frustrated motion is due to antagonizing motors ([Figure 4C](#)). Anti-parallel bundle traces exhibited a ramp where the motors began generating force until they stalled out against the trap and plateaued ([Figure 4D](#)). This is similar to Eg5 in microtubule overlaps [25], except the plateau force here remained close to stall forces for individual motors ( $3.7 \pm 1.0$  pN,  $n = 17$ ). The corresponding translation velocity was  $0.44 \pm 0.19$  nm s<sup>-1</sup> ( $n = 17$ ). Also, only 28% of the bundles were anti-parallel in orientation while the other 72% were parallel. This observation is consistent with Drechsler and McAinsh, who showed that Kif15 has a 70% bundling bias for parallel microtubules in the presence of ATP [38].

The same bundling experiment was performed with N700 ([Figure S3](#)) behaving similarly to Kif15. There was a 69% bundling bias for the parallel orientation that lacked force generation, whereas, in anti-parallel bundles, the force profile showed

a ramp followed by a plateau, as with Kif15. Since Kif15 and N700 exhibited similar capabilities, Coil-1's microtubule-bundling role was further investigated through two experiments: (1) bundling with a construct lacking Coil-1 (N420) and (2) with N700 (including Coil-1) but with digested microtubules ([Figure S4](#)). Microtubules did not bundle in both cases. Therefore, the Coil-1-E-hook interaction is necessary for bundle formation by Kif15. Together, these results reveal that Kif15 can generate force between anti-parallel microtubules while net progress in parallel microtubules is minimal with frustrated oscillations around baseline.

### Kif15 Contains a Force-Feedback Mechanism

The low plateau force in anti-parallel bundles indicates that Kif15 may have a self-governing mechanism that limits its force-generating capabilities in large numbers. To test this idea, a combined microtubule-gliding/optical tweezer assay was developed (see the [STAR Methods](#)) to compare Kif15, Eg5 ([Figure 5](#)), and N700 ([Figure S5](#)). Eg5 behaved similarly to what was found previously, where many motors generated a large amount of force ([Figure 5B](#), blue) [25]. Force plateaus of 20–30 pN were observed ( $n = 8$ ), where some traces reached the stall, fell back briefly with jagged trajectories, and continued to glide persistently. In contrast, Kif15 ( $n = 8$ ) behaved similarly as at very low concentration in the bundle assay. There was a slow and smooth force ramp that finally plateaued minutes later at 5–6 pN. N700 behaved similarly to Kif15 ([Figure S5B](#)).



### Figure 3. Coil-1-Binding Assay

(A) Assay design (STAR Methods).

(B) Coil-1/microtubule lifetime distribution, averaging  $5.6 \pm 1.6$  s and  $24.8 \pm 7.9$  s ( $n = 109$ ).

(C) Force at rupture, averaging  $6.1 \pm 2.0$  pN and  $10.81 \pm 1.8$  pN ( $n = 109$ ).

(D) E-hook digestion confirmation using SDS-PAGE through separation of alpha- and beta-tubulin bands (ladder, control [sample buffer and water], microtubules [stock and 10 $\times$  diluted], digested microtubules [stock and 10 $\times$  diluted]).

(E) Coil-1/digested microtubule lifetime, averaging  $5.2 \pm 1.4$  s ( $n = 49$ ), is comparable to the lower value for normal microtubule (B).

(F) Digested microtubule rupture force, averaging  $3.4 \pm 1.4$  pN ( $n = 49$ ).

(G) Example ruptures on normal (blue) and digested microtubules (red).

(H) Coil-1 lifetime versus rupture force on normal ( $R^2 = 0.77$ ) and digested microtubule ( $R^2 = 0.68$ ). Error bars, SEM.

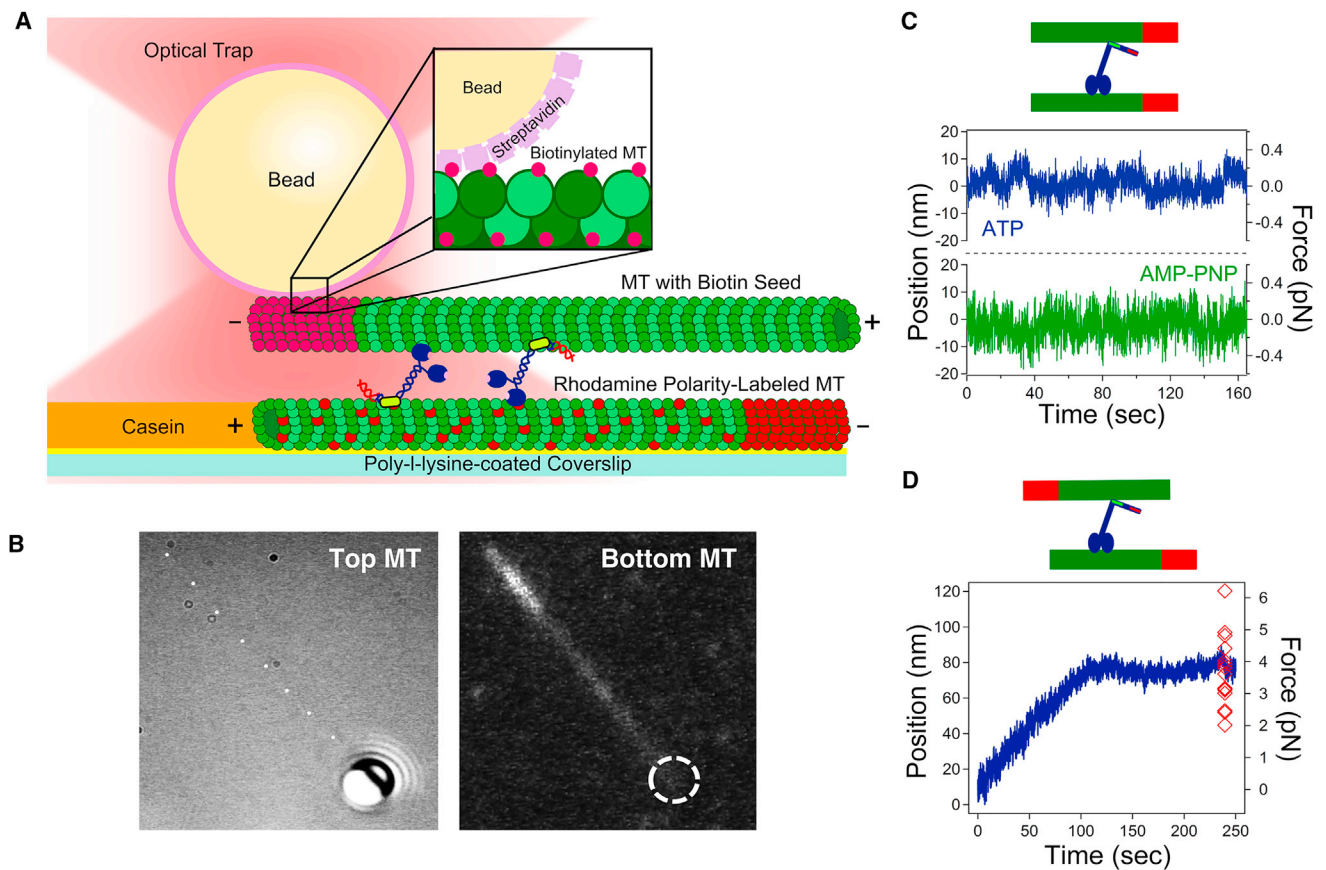
See also Figure S2.

Due to the non-specific nature of motor binding to the glass surface, both the motor heads and Coil-1 can help recruit microtubules to the surface to subsequently glide. The same trace patterns between this gliding assay and the bundle assay revealed that the distributions of motor orientations were most likely similar.

To better understand the plateauing behavior, we developed a stochastic model of microtubule gliding by Kif15 (STAR Methods). The trap stiffness, three-state force-velocity relation, Kif15 stall force, backstep probability, and tail (Coil-1) rupture force were adopted from experimental values. Model parameters unavailable from experiment were adjusted so that resulting behaviors matched semiquantitatively with experiment. We also incorporated “tethered tails” whose opposite motor domain was

attached to the substrate and immobile. This mimicked the situation where Coil-1 was bound to the microtubule in the gliding assay (Figure 5A). Such scenarios may also arise in microtubule bundles as motor domains waiting for ATP binding are in rigor states (Figure 5C).

We first ran the simulation without backstepping and tail rupturing. The microtubule trajectory followed a sawtooth pattern caused by walking until stall, detachment, and return to the origin (Figure 5D). With backstepping, the force rapidly plateaued, indicating that a balance between forward and backward steps was established (Figure 5E). The rapid rise and noisy force trace qualitatively corresponded to Eg5 where both ends of the motor walk (hence, a low chance of forming a tether), which also can backstep (Figure 5B) [24]. On the other hand, when tail



**Figure 4. Microtubule Bundle Assay**

(A) Assay schematic (STAR Methods).

(B) Top microtubule (DIC) with streptavidin bead bound to the biotinylated minus end, bundled to the bottom microtubule (fluorescence). Dashed circle denotes bead location.

(C) Parallel bundles yielded baseline force generation. With AMP-PNP, only thermal noise is present. Kif15 has a 72% parallel bundle bias ( $n = 43$ ).

(D) Anti-parallel bundles yielded a force ramp and plateau at a stall force similar to a single motor ( $n = 17$ ). Red diamonds, individual stall forces.

See also Figures S3 and S4.

rupturing was activated, the force ramped more slowly and the profile became smoother (Figures 5F and 5G). For this, back-stepping was not essential, but it lowered the plateau force slightly due to the additional force relaxation (Figures 5F and 5G).

These results provide evidence for Kif15 having a force-feedback mechanism that limits force generation and fluctuation. Tethering by Coil-1 is essential for this feedback. Coil-1 provides support as motor domains walk and transport microtubules. For motor domains awaiting ATP, the corresponding Coil-1, with its high rupture force, serves as a tether that limits microtubule gliding, manifesting a force plateau on the bead.

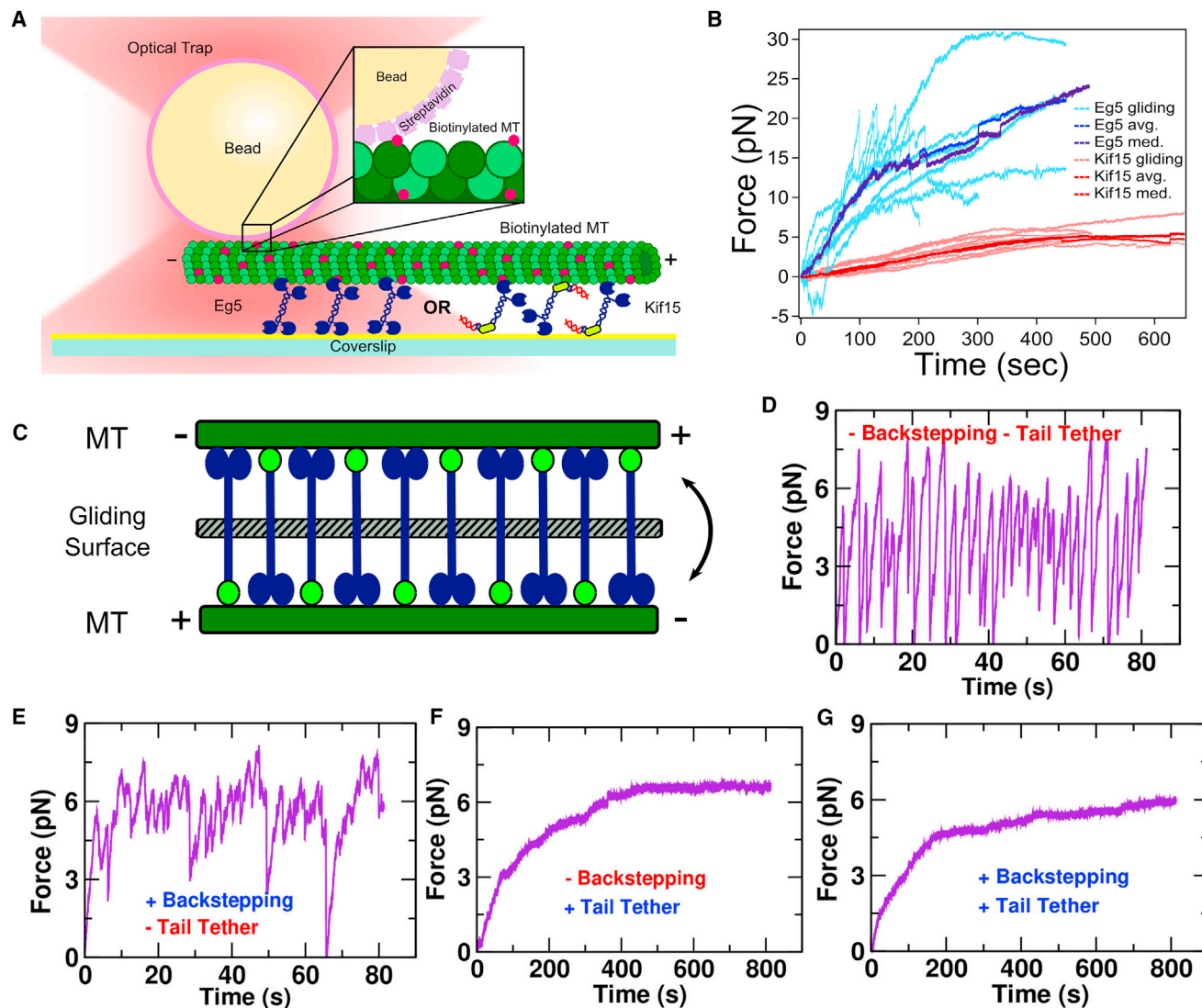
## DISCUSSION

In human cells, it is unknown how Kif15 generates centrosome separation forces necessary to drive spindle assembly [13, 17]. Since Eg5 promotes spindle assembly through anti-parallel microtubule-microtubule sliding [2], the prevailing hypothesis is that Kif15 produces outward force through a similar mechanism, prompting several models [13, 26, 27]. One model posits that Kif15 may exist as a tetramer in solution and thus is Eg5-like

[26]. However, our measurements reported here (Figure S1) and in our previous works [16, 27] show that our Kif15 constructs are homodimers in solution and in cells. A recent study from Brouwers et al. supports that Kif15 is a dimer in solution [28]. A second model suggests that Kif15 may complex with TPX2, enabling microtubule-microtubule crosslinking and sliding [13]. Recognizing that Kif15 contains Coil-1, we previously proposed a third model wherein Kif15 dimers drive microtubule-microtubule sliding [27] similarly to fly kinesin-14 (Ncd) [39] and yeast kinesin-8 (Kip3) [40]. This is consistent with the finding that a minimal Kif15 construct (N700) drives microtubule-microtubule sliding [27]. Here, we show that non-truncated Kif15 also catalyzes microtubule-microtubule sliding when anti-parallel. In conjunction with our optical trapping data, our observations provide a biochemical explanation for how Kif15 promotes spindle assembly and yield insight into the functional relationship between Kif15 and Eg5 within the spindle.

In contrast to a single Eg5 tetramer that walks on both anti-parallel microtubules, Kif15 most likely “runs in place” between two microtubules, based on Coil-1 having a rupture force at least 2-fold greater than Kif15’s stall. Strong Coil-1/microtubule





**Figure 5. Combined Microtubule-Gliding/Optical Tweezer Assay**

(A) Assay schematic (STAR Methods).

(B) Loading traces of gliding microtubules on Eg5 (blue,  $n = 8$ ) and Kif15 (red,  $n = 8$ ). Eg5 generates force, sliding faster ( $0.1 \pm 0.02$  pN/s) than Kif15 ( $0.01 \pm 0.006$  pN/s). Kif15 behaves similarly as in anti-parallel bundles (Figure 4D).

(C) Model schematic. Simulation results can be interpreted as a gliding microtubule or anti-parallel bundle (Results).

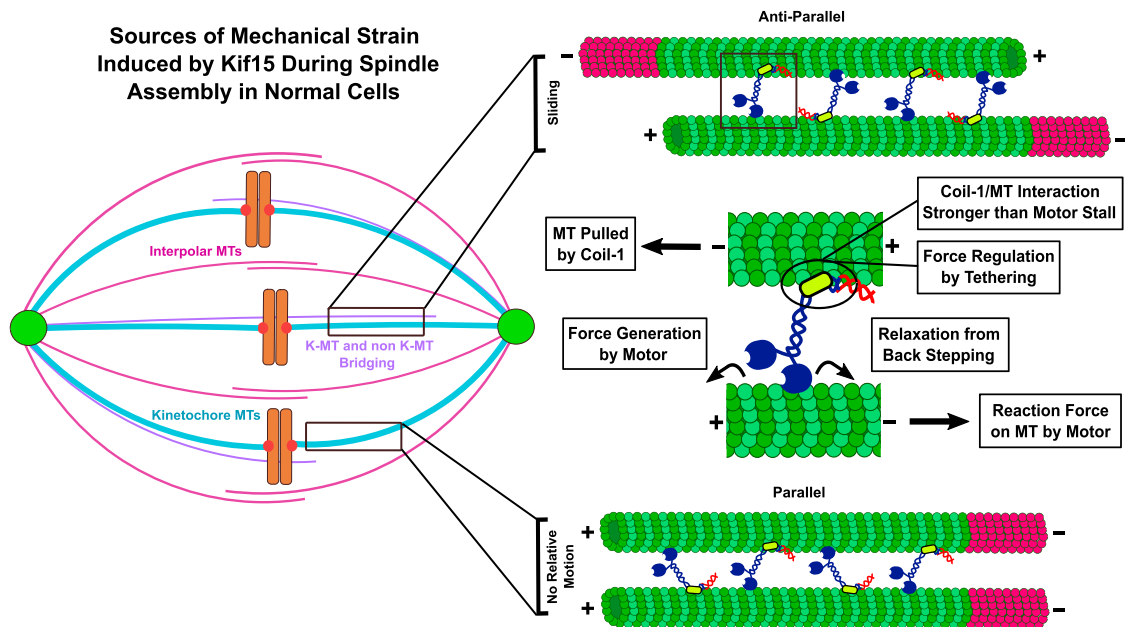
(D–G) Simulated sliding with different model components (STAR Methods) such as (D) no inclusion of backsteps or tethered tails, (E) inclusion of backsteps but not tethered tails, (F) inclusion of tethered tails but not backstepping, and (G) inclusion of both backsteps and tethered tails. Simulated system contains 5 Kif15 motors. In (F) and (G), 5 tethers are present with Coil-1 binding to the microtubule at 6.1-pN rupture force while the other end is stationary. Only with tethers are slow ramping and reduced force fluctuation observed.

See also Figure S5.

binding is most likely electrostatic, as E-hook removal significantly reduces the strength of the interaction. In an anti-parallel bundle, Kif15 exerts force directed toward the minus end of each microtubule, regardless of whether its motor or Coil-1 domain is bound, causing the microtubules to slide apart (Figure 6). In the parallel case, a Kif15 motor head pushes a microtubule toward its minus end, whereas Coil-1 pushes it to the plus end as its motor domain on the other microtubule walks, causing both microtubules to become locked (Figure 6). This model also mirrors the mechanism proposed for fly kinesin-14,

a dimeric motor with a non-motor microtubule-binding site on its tail [39, 41].

We also found distinct regulation of force generation between anti-parallel microtubule bundles by Kif15. Force ramps gradually over a period that is much longer than individual motor dwell times to a plateau not significantly larger than the motor's stall force. Furthermore, force fluctuation is much smaller than observed for Eg5 (Figure 5). Our simulation shows that force regulation by an ensemble of Kif15s is determined mainly by the tethering effect of Coil-1. Although backstepping contributes



**Figure 6. Model for Kif15 Function in Microtubule Bundles**

Force generated by Kif15 transmits between microtubule bundles via Coil-1 and the motor head. In the anti-parallel case, the motors collectively slide microtubules apart. In the parallel case, motors yield no relative movement (Discussion).

to force relaxation, its timescale is comparable to the forward stepping time; force fluctuates over a timescale comparable to the motility of individual motors (several seconds). Also, the force fluctuation amplitude is large since it is determined essentially by the motility and detachment of individual motors (Figure 5E). This is the case even with tail rupturing since unbinding of the motor domain occurs more quickly and at lower force. On the other hand, if the motor unbinds from the microtubule mainly via tail rupturing (a tethered case), the tethered tails serve as transient crosslinks between two microtubules, slowing down microtubule sliding and suppressing force fluctuation (Figures 5F and 5G). A modest level of rupture force is crucial since a very high tether rupture force would correspond to a static crosslink that prevents microtubule sliding.

Force regulation by an ensemble of Kif15 differs significantly from Eg5 [25]. Having motor domains on both ends, force regulation by an Eg5 ensemble occurs on a timescale comparable to that of individual motors. It is, perhaps, for this reason that Eg5 and Kif15 differ in spindle assembly efficiency. In contrast to Eg5, Kif15 is poor at driving centrosome separation, even under conditions where the motor is overexpressed; spindles remain monopolar for long periods of time, potentially storing energy, and “pop open” when reaching a force threshold [13, 17]. The difference in force-producing behaviors of Eg5 and Kif15 also has implications for how the motors distribute within the metaphase spindle. Under normal conditions, Kif15 concentrates on kinetochore microtubules, whereas Eg5 accumulates on spindle microtubules indiscriminately. Ensembles of Eg5 can easily produce forces in excess of 6 pN within anti-parallel overlaps, with single molecules each generating  $\sim 1.5$  pN [25]. Linear scaling of motors with force implies that small numbers ( $\sim 4$ ) of Eg5 motors can displace Kif15 molecules from the anti-parallel overlap,

a force-feedback mechanism that may cause Eg5 and Kif15 to associate with distinct spindle microtubule geometries [17].

What is the function(s) of Kif15 on kinetochore microtubules? In HeLa cells, Kif15 is required for spindles to remain bipolar at metaphase [13, 15]. Similarly, Kif15 slows K51-triggered collapse of metaphase spindles in RPE-1 cells [42]. These data strongly suggest that Kif15 not only helps bundle microtubules but also somehow generates an outward-directed force within the spindle, even while restricted to kinetochore microtubules. Since Kif15 cannot generate net sliding forces within parallel bundles, we propose that Kif15 motors mechanically link non-kinetochore microtubules to kinetochore microtubules and slide them apart only when anti-parallel (Figure 6). Near the centromere, such microtubules constitute “bridging fibers,” which link sister kinetochore fibers and balance inter-kinetochore tension [43]. We speculate that mechanical coupling of non-kinetochore and kinetochore microtubules is more pervasive throughout the spindle, as Kif15 is uniformly distributed along kinetochore microtubules [17]. The distinct function of Kif15 in parallel kinetochore microtubules, its structural and mechanical differences from Eg5, and the jackknifing effect [17] upon rescuing spindle assembly demonstrate that Kif15 contributes uniquely to spindle dynamics.

In summary, dimeric Kif15 regulates force generation differently depending on microtubule orientation. Essential to its force-regulating capability is the fine physical balance between the motor head motility properties and the Coil-1/microtubule interaction. Physiologically, Kif15 localizes to kinetochore microtubules to aid in stability and regulate length through plus end tracking, as proposed elsewhere [38], as well as antagonize motor movement that only allows for subtle, well-regulated displacement, as shown here. Kif15 can rescue the function of

inhibited Eg5 by utilizing Coil-1 in conjunction with its motor heads to build up mechanical strain and slide anti-parallel microtubules apart, building a bipolar spindle that is necessary for successful mitosis. This mechanism demonstrates the therapeutic importance of Kif15, whose inhibition in tandem with an Eg5 inhibitor could prove to be more effective in the clinic.

## STAR★METHODS

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## SUPPLEMENTAL INFORMATION

Supplemental Information includes five figures and two movies and can be found with this article online at <http://dx.doi.org/10.1016/j.cub.2017.08.018>.

## AUTHOR CONTRIBUTIONS

D.N.R. was involved in all aspects of the work, including assay development, performing experiments, data analysis, and manuscript preparation. E.G.S., D.N.R., and R.O. expressed and purified the constructs. E.G.S. performed microtubule-gliding fluorescence assays. D.K.D. and Z.V. aided in assay design. M.S.D. aided in developing the protocol for making digested microtubules. W.H., M.J.L., D.N.R., and R.O. designed the simulation. W.H. developed and performed the simulation. D.N.R., M.J.L., R.O., and W.H. prepared the manuscript.

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## STAR★METHODS

## KEY RESOURCES TABLE

REAGENT or RESOURCE	SOURCE	IDENTIFIER
<b>Antibodies</b>		
His Tag Antibody, mAb	GenScript	Cat#A00186-100; RRID: AB_914704
Penta-His Biotin Conjugate	QIAGEN	Cat#34440
<b>Bacterial and Virus Strains</b>		
Bac-to-Bac Baculovirus Expression System	Thermo Scientific	Cat#10359-016
BL21 DE3	Novagen	Cat#69450
<b>Chemicals, Peptides, and Recombinant Proteins</b>		
Kif15	This paper	N/A
N700	This paper	N/A
N420	This paper	N/A
Coil-1	[27]	N/A
Eg5	[16]	N/A
Phusion DNA Polymerase	Thermo Scientific	Cat#F530L
Bovine Tubulin	Cytoskeleton	Cat#TL238
PIPES	Sigma	Cat#P-1851
EGTA	Sigma	Cat#E-4378
MgCl <sub>2</sub>	Mallinckrodt	Cat#H590
GTP	Cytoskeleton	Cat#BST06
ATP	Sigma	Cat#A26209
Bovine Tubulin	PurSolutions	Cat#1001
Taxol	Cytoskeleton	Cat#TXD01
Subtilisin	Sigma	Cat#P8038
PMSF, phenylmethanesulfonyl fluoride	Sigma	Cat#P7626
GMPCPP	Jena Bioscience	Cat#NU-405L
Rhodamine Tubulin	Cytoskeleton	Cat#TL590M
Biotinylated Tubulin	Cytoskeleton	Cat#T333P-A
Blotting Grade Blocker (casein)	BioRad	Cat#1706404
Glucose Oxidase	Sigma	Cat#G2133
β-D-Glucose	Sigma	Cat#G8270
Catalase	Sigma	Cat#C40
Streptavidin beads	Spherotech	Cat#SVP-05-10
Sulfo-NHS	ThermoScientific	Cat#24510
EDC	ThermoScientific	Cat#22980
Ethanolamine	Sigma	Cat#E9508
Poly-L-lysine	Sigma	Cat#P8920
<b>Oligonucleotides</b>		
5'-biotin-TATTGCGTTTCCTCGGTTTC-3'	IDT	N/A
5'-amine-TTGAAATACCGACCGTGTGA-3'	IDT	N/A
Kif15_N420_5'_IA: GCAGCGGCCTGGTGCCGCGCG GCAGCCATATGGCACCCGGCTGCAAAC	IDT	N/A
Kif15_N420_3'_IA: CGGGCTTTGTTAGCAGCCGGAT CCTCGAGCTAAGACTTCTTTCTGTTTC	IDT	N/A
Kif15_pFB_5': GCAGCGGCCTGGTGCCGCGCGCGC AGCCATATGGCACCCGGCTGCAAAC	IDT	N/A

(Continued on next page)

**Continued**

REAGENT or RESOURCE	SOURCE	IDENTIFIER
Kif15_FL_(GGS) <sub>2</sub> _GFP_3': CTCGCCCTTGCTCACC ATTGATCCTCCTGATCCTCCAGATTCACCTCTTTTCTTTTC	IDT	N/A
Kif15_FL_(GGS) <sub>2</sub> _GFP_5': GAAAAGAAAAGAAGTG AATCTGGAGATCAGGAGGATCAATGGTGAGC AAGGGCGAG	IDT	N/A
GFP_His6_pFB_3': AGCTTGGTACCGCATGCCTCGAGAC TGCAGTCAGTGATGGTGATGGTGATGCTGTACAGC TCGTCCATG	IDT	N/A
Kif15_700_(GGS) <sub>2</sub> _GFP_3': CTCGCCCTTGCTCACCATT GATCCTCCTGATCCTCCAATGGCCTCAAAGCTTG	IDT	N/A
Kif15_700_(GGS) <sub>2</sub> _GFP_5': CAAGCTTTTGAGGCCATTGG AGGATCAGGAGATCAATGGTGAGCAAGGGCGAG	IDT	N/A
Recombinant DNA		
pET-15	Novagen	Cat#69661
M13mp18	[44]	N/A
pFASTBAC1	Thermo Scientific	Cat#10712-024
Software and Algorithms		
MATLAB	Mathworks	N/A
Stochastic Kinesin Simulation	This paper	N/A
Other		
Micro Bio-Spin 30 Column	BioRad	Cat#7326250

**CONTACT FOR REAGENT AND RESOURCE SHARING**

Further information and requests for resources and reagents should be directed to and will be fulfilled by the Lead Contact, Matthew Lang ([matt.lang@vanderbilt.edu](mailto:matt.lang@vanderbilt.edu)).

**EXPERIMENTAL MODEL AND SUBJECT DETAILS**

No cell or animal experiments were conducted.

**METHOD DETAILS****Molecular biology/baculovirus construction**

pET15-Kif15-Coil-1 was described previously [27]. pET15-Kif15-N420 was constructed by isothermal assembly. A PCR fragment encompassing Kif15 amino acids 1-420 was generated with Phusion DNA polymerase (Thermo) using the following conditions: 1) 98°C, 30 s; 2) 98°C, 10 s; 3) 56°C, 30 s; 4) 72°C, 90 s; 5) repeat steps 2-4 30 times; 6) 72°C, 10 min. The fragment was purified and assembled into pET15 (Novagen) restricted with *NdeI* and *XhoI*.

pFASTBAC1-Kif15-GFP (pRO1221) and pFASTBAC1-Kif15-N700-GFP (pRO1222) were constructed by 3 part isothermal assembly into the Bam H1 and PstI sites of pFASTBAC1 (ThermoFisher Scientific). Kif15 and GFP coding sequences were PCR amplified using conditions described above, but with varying elongation times (step 4). Primers for amplification (see [Key Resources Table](#)) included: 1) a (GGS)<sub>2</sub> linker in between Kif15 and a 3' end-positioned GFP; and 2) a hexahistidine tag downstream of GFP. pRO1221 and pRO1222 were used with the Bac-to-Bac system (ThermoFisher Scientific) to create baculoviruses that express Kif15-FL-GFP-His<sub>6</sub> and Kif15-N700-GFP-His<sub>6</sub>, respectively.

pFASTBAC-HTc-Eg5-WT was constructed as described previously [16]. The Eg5 coding region from pEGFP-C1-Eg5-WT was amplified and assembled into Sall-EcoRI-restricted pFASTBAC-HTc (ThermoFisher Scientific) by isothermal assembly. This was used with the Bac-to-Bac system (Invitrogen) to create baculoviruses that express His<sub>6</sub>-Eg5-WT.

**Protein expression and purification**

His<sub>6</sub>-Kif15-N420 and His<sub>6</sub>-Kif15-Coil-1 were expressed in and purified from BL21DE3 cells. Both constructs were expressed for 4 hr in cells cultured at 18°C with 0.4 mM IPTG. For purification, cells were pelleted and resuspended in lysis buffer (PNI [50 mM sodium phosphate, 500 mM NaCl, 20 mM imidazole], 5 mM β-mercaptoethanol, and 1% NP40, and protease inhibitors [1 mM phenylmethylsulfonyl fluoride, 1 mM benzamide, and 10 μg/mL each of leupeptin, pepstatin, and chymostatin]). All buffers to purify

His<sub>6</sub>-Kif15-N420 additionally contained 50 μM MgATP. Lysate was incubated with 1 mg/mL lysozyme for 30 min, sonicated, and clarified by centrifugation at 35,000 rpm for 1 hr in a Ti 45 rotor (Beckman). ~3 mL of Ni<sup>2+</sup>-NTA agarose (QIAGEN) was incubated with the supernatant for 1 hr at 4°C, and then washed with wash buffer (PNI, 5 mM β-ME, 10% glycerol). Protein was eluted with PNI, 5 mM β-ME, and 180 mM imidazole. His<sub>6</sub>-Kif15-Coil-1 was desalted with a PD10 column (GE Healthcare) equilibrated with 10 mM K-HEPES, pH = 7.7, 100 mM KCl, 1 mM DTT, and 20% sucrose. His<sub>6</sub>-Kif15-N420 was subjected to size exclusion chromatography on a Superdex 200 column equilibrated in 10 mM K-HEPES, pH = 7.7, 100 mM KCl, 1 mM DTT, and 0.1 mM MgATP. For both, peak fractions were pooled, aliquoted, frozen in liquid nitrogen, and stored at –80°C.

Kif15-FL-GFP-His<sub>6</sub>, Kif15-N700-GFP-His<sub>6</sub>, and His<sub>6</sub>-Eg5-WT were expressed in Sf9 cells cultured at 27°C for 72 hr. For purification, cells were pelleted and resuspended in lysis buffer (PNI, 5 mM β-mercaptoethanol (β-ME), and 1% NP40, and protease inhibitors [1 mM phenylmethylsulfonyl fluoride, 1 mM benzamide, and 10 μg/ml each of leupeptin, pepstatin, and chymostatin]). Lysate was incubated on ice for 15 min, sonicated, and clarified by centrifugation at 35,000 rpm for 1 hr in a Ti 45 rotor (Beckman). ~2 mL of Ni<sup>2+</sup>-NTA agarose (QIAGEN) was incubated with the supernatant for 1 hr at 4°C, and then washed extensively with wash buffer (PNI, 5 mM β-ME, and 50 μM MgATP). Protein was eluted with PNI, 5 mM β-ME, 0.1 mM MgATP, and 180 mM imidazole, and peak fractions subjected to desalting with a PD10 column (GE Healthcare) equilibrated in 10 mM K-HEPES, pH = 7.7, 300 mM KCl, 1 mM DTT, and 0.1 mM MgATP. Protein concentrations were determined using Bradford assays and take into account that Kif15 exists as a dimer in solution and Eg5 exists as a tetramer in solution. Powdered sucrose was added to 20% w/v. Protein was aliquoted, frozen in liquid nitrogen, and stored at –80°C.

### Microtubule preparation

Purified bovine tubulin, purchased from Cytoskeleton (TL238), was reconstituted in 25 μL PEM80 buffer (80 mM PIPES (Sigma P-1851), 1 mM EGTA (Sigma E-4378), 4 mM MgCl<sub>2</sub> (Mallinckrodt H590), pH adjusted to 6.9 with KOH) supplemented with 1 mM GTP (Cytoskeleton BST06) and kept on ice. Purified tubulin from PurSolutions (bovine, 1001) was also used and reconstituted in the supplied polymerization buffer. 13 μL PEM104 buffer (104 mM PIPES, 1.3 mM EGTA, 6.3 mM MgCl<sub>2</sub>, pH adjusted to 6.9 with KOH), 2.2 μL 10 mM GTP, and 2.2 μL DMSO were mixed. 4.8 μL of 10 mg/mL tubulin were added to the mixture and allowed to incubate for 40 min at 37°C. Subsequently, 2 μL of stabilization solution (STAB, 38.6 μL PEM80, 0.5 μL 100 mM GTP, 4.7 μL 65 g/L Na<sub>3</sub> (Sigma S-8032), 1.2 μL 10 mM Taxol (Cytoskeleton TXD01), 5 μL DMSO (Cytoskeleton)) was added to the stock microtubule solution at room temperature.

Digested microtubules were made by removing the C-terminal E-hook of microtubules with subtilisin. 7.5 μL of pre-formed microtubules were mixed with 0.75 μL of 20 μM subtilisin (Sigma P8038) and was allowed to incubate at 37°C for 40 min. To stop digestion, 0.8 μL of 20 mM PMSF (phenylmethanesulfonyl fluoride, Sigma P7626) in DMSO was added to the digested microtubule mixture. 2 μL of STAB solution was then added to the digested microtubules at room temperature.

Polarity-marked microtubules were prepared by making a brightly fluorescent microtubule seed and polymerizing dimmer tubulin from that nucleation point. The microtubule seed was formed using GMPCPP, a non-hydrolysable analog of GTP (Jena Bioscience NU-405L). Rhodamine-labeled tubulin (Cytoskeleton, TL590M) was used in different concentrations to denote the bright seed from the dimmer elongation. First, the seed was polymerized by mixing 13 μL PEM104, 2.2 μL 10 mM GMPCPP, 2.2 μL DMSO, 4 μL non-labeled tubulin (10 mg/mL), and 1 μL rhodamine-labeled tubulin (10 mg/mL). The seed mixture was incubated at 37°C and allowed to incubate for 40 min. The elongation solution was made by mixing 13 μL PEM104, 2.2 μL 10 mM GTP, 2.2 μL DMSO, 2 μL non-labeled tubulin (10 mg/mL), and 1.5 μL rhodamine-labeled tubulin (1 mg/mL). The elongation mixture was incubated at 37°C for 1 min to ensure that the mixture was at least at room temperature. After a minute, 1.5 μL of the seed mixture was added to the elongation mixture and allowed to incubate at 37°C for 40 min. Subsequently, 2 μL of STAB solution was added to the polarity-marked microtubules at room temperature.

### Microtubule gliding assays

Microtubule gliding assays for Kif15 were performed as described previously [16, 27]. Flow cells were constructed with double-stick tape, and motor was added at stock concentration (1.1 μM Kif15; 0.88 μM Eg5) for 3 min and X-rhodamine-labeled GMPCPP microtubules (1:9 labeled:unlabeled) at 300 nM tubulin in BRB80 for 3 min. Flow cells were washed between each addition with 3 volumes of BRB80, 50 mM KCl, 1 mM MgATP, and 500 μg/mL casein. After the final addition, flow cells were washed with 3 volumes of BRB80, 50 mM KCl, 1 mM MgATP, 500 μg/mL casein, and oxygen scavenging mix (200 μg/mL glucose oxidase, 35 μg/mL catalase, 25 mM glucose, 70 mM β-ME). Microtubule gliding was recorded at 5 s intervals by time-lapse microscopy.

Combined gliding and optical trapping assays were constructed in the same manner except 1:9 biotinylated microtubules were used in place of rhodamine microtubules and 1.25 μm streptavidin beads (Spherotech) were added to the final buffer addition. Beads were trapped in solution and actively bound to the biotinylated microtubules for force measurement.

### Bead functionalization

Coil-1 was tethered to 0.44 μm streptavidin polystyrene beads (Spherotech – SVP-05-10) via a 1,010 bp DNA linker functionalized with biotin and a terminal amine. The 1,010 bp DNA linkers were created using PCR and the M13mp18 plasmid template using the following conditions: 1) 98°C, 30 s; 2) 98°C, 10 s; 3) 49°C, 30 s; 4) 72°C, 90 s; 5) repeat steps 2-4 35 times; 6) 72°C, 10 min.

All primers were ordered from Integrated DNA Technologies (IDT). One 5' biotinylated primer (forward, 5'-biotin-TATTGCGTTTCCTCGGTTTC-3') and one 5' amine-functionalized primer (reverse, 5'-amine-TTGAATACCGACCGTGTGA-3') were used with the M13mp18 template. After PCR, the amine-functionalized end of the tethers were crosslinked to anti-His tag antibody (GenScript – A00186-100) using sulfo-NHS/EDC chemistry. EDC (1-ethyl-3-(3-dimethylaminopropyl)carbodiimide hydrochloride, Thermo Scientific – 22980), Sulfo-NHS (N-hydroxysulfosuccinimide, Thermo Scientific – 24510), ethanolamine (Sigma – E9508), and PBS (1x, pH 7.4) were used in this reaction. The DNA linkers were then purified using Micro Bio-Spin 30 columns (Biorad). Streptavidin beads, DNA linker (33 ng/ $\mu$ L), and Coil-1 (1 nM) diluted in assay buffer (AB, 80 mM PIPES, 1 mM EGTA, 4 mM  $MgCl_2$ , 1 mM DTT, 20  $\mu$ M Taxol, 1 mg/mL casein, 1 mM ATP) were incubated together for 1 hr at 4°C on a rotator to create Coil-1 tethered beads.

Motor functionalized beads were created by binding the C terminus of the motor to the bead via a His-tag linkage. 0.44  $\mu$ m streptavidin polystyrene beads (Spherotech – SVP-05-10) were incubated with 0.2 mg/mL biotinylated anti-His tag antibody (QIAGEN – 34440) to create anti-His tag coated beads. The beads were washed with PBS (1x, pH 7.4) 4 times by centrifuging at 10,000 rpm for 6 min to remove any unreacted biotinylated anti-His. The beads were then incubated with 1 nM of motor diluted in AB for 1 hr at 4°C on a rotator in the presence of an oxygen scavenging system (5 mg/mL  $\beta$ -D-glucose (Sigma G8270), 0.25 mg/mL glucose oxidase (Sigma G2133), and 0.03 mg/mL catalase (Sigma C40)).

### Single molecule optical trapping assays

A flow cell that holds a volume of  $\sim$ 15  $\mu$ L was assembled using a microscope slide, etched coverslips, and double-sided sticky tape. Before assembly, etched coverslips were incubated in a solution of 100  $\mu$ L poly-L-lysine (PLL, Sigma P8920) in 30 mL ethanol for 15 min. The coverslip was then dried with a filtered air line. After flow cell assembly, microtubules were diluted 150 times from the stock in a solution of PemTax (1  $\mu$ L 10 mM Taxol in 500  $\mu$ L PEM80). The diluted microtubules were added to the flow cell via capillary action and allowed to incubate to the PLL surface for 10 min. Unbound microtubules were then washed out with 20  $\mu$ L PemTax. A solution of casein (Blotting-Grade Blocker, Biorad 1706404) diluted in PemTax (1:8 mixture) was then added to the flow cell and allowed to incubate for 10 min to block the remainder of the surface to prevent non-specific binding. We found that the assay was very sensitive to the grade of casein used to block the surface and found optimal results with the blotting-grade blocker used here. After the incubation, the flow cell was washed with 50  $\mu$ L PemTax and 80  $\mu$ L assay buffer (AB). 20  $\mu$ L of the bead solution described above (either tethered or with full motor) that had incubated for 1 hr was then added to the flow cell.

Optical trapping measurements were obtained using a custom built instrument with separate trapping and detection systems. The instrument setup and calibration procedures have been described previously [32]. Briefly, beads were trapped with a 1,064 nm laser that was coupled to an inverted microscope with a 100x/1.3 NA oil-immersion objective. Bead displacements from the trap center were recorded at 3 kHz and further antialias filtered at 1.5 kHz. Position calibration and trap stiffness measurements were obtained using custom Labview programs.

To ensure that we were at the single molecule limit for both the binding assay and motility assay, the protein-bead ratio was adjusted so that fewer than half of the beads trapped and tested on microtubules showed binding, actually having 5%–10% binding the majority of the time.

In the binding assay, beads were trapped in solution and brought close to surface-bound microtubules to allow for binding of Coil-1. Once a tether was confirmed through visual inspection in DIC mode, the tether was centered by an automated two axis piezo-stage centering routine. Afterward, the bead was again trapped and the piezostage was translated to load the interaction with force. Rupture of the Coil-1-microtubule interaction was confirmed by the bead diffusing away from the microtubule after the trap is turned off once the measurement was complete. A single tether was characterized to have a single break back to baseline in the measurements. This was also the case for the directional pulling assay with polarity-marked microtubules. The exception is that the orientation of the microtubule was checked in fluorescence mode, noted, and then after switching back to DIC mode, the piezostage was translated in the direction of testing (either toward the plus end (dimly fluorescent elongation) or minus end (brightly fluorescent seed) of the microtubule).

In the motor motility assay, a motor-coated bead was trapped in solution and subjected to position calibration and trap stiffness Labview routines. Afterward, the bead was brought close to a surface-bound microtubule to allow for binding. Bead position displacement and force generation were measured for single motor-bound beads.

This is very similar to the unloaded velocity assay except for when the bead is brought close to the microtubule, the trap and detection lasers are turn off, and the bead motion on the microtubule is video-tracked with a DAGE CCD camera. Custom MATLAB code based on a cross-correlation method was used to track the bead positions over time [45].

### Microtubule bundle assays

Microtubule bundles were generated by adhering a rhodamine-labeled polarity-marked microtubule to a coverslip surface (substrate microtubule) that was further blocked with casein. A motility mixture consisting of a known concentration of motor, polarity-marked microtubules with a biotinylated seed at the minus end (cargo microtubule), and streptavidin coated beads was then added to the flow cell to allow for spontaneous bundle formation through the motors. A free, streptavidin-coated



bead was trapped in solution and brought to an apparent microtubule bundle. Bundles appear slightly thicker than normal isolated microtubules under DIC microscopy. Bead binding to an end verifies that a motor-formed bundle was found as beads only bind the biotinylated minus ends of the cargo microtubules. Control experiments in the absence of motor did not bind microtubules.

### Single molecule photobleaching assay

Single molecules of FL-Kif15-GFP were imaged at 200 pM in assay buffer through non-specific adsorption to an etched coverslip in a flow cell. The protein was allowed to incubate for 10 min, and then unbound motor was washed out with 3 volumes of assay buffer. Images were acquired at 8.66 Hz using TIRF microscopy equipped with an EMCCD camera. GFP was excited with 488 nm at an exposure time of 0.1 s. Locating individual fluorescent FL-Kif15-GFP molecules for photobleaching analysis was performed from analysis of video frames using custom software written in MATLAB (Mathworks) [46].

### Data analysis

Nanometer position and piconewton force values were measured using calibration data and trap stiffness measurements from each bead before data acquisition. Those traces were visualized in custom-built MATLAB code to determine overall signature of the traces as well as the stall force measurements. Other scripts were used to determine lifetimes, velocities, and local force-velocity relationships. Step-finding code based on a sliding Student's *t* test was used to determine the boundaries of each step to denote a dwell time in between, as well as allow for measuring varied step sizes [44]. A dwell was defined as constant position over time in between steps. In this code, a dwell was measured if the change in the moving average of position was less than 3 nm. This step threshold was chosen due to the defined step sizes of most kinesins (around 8 nm), but could allow for variability without detecting steps from noise (measurements less than 3 nm). Accounting for steps less than 3 nm shows a marked increase in number of steps. However, upon visual inspection of how the trace was been analyze by the code for accuracy, it was found that these steps below 3 nm were indeed noise and therefore not accounted for in averaging.

Force change correlates with the distance the bead has been displaced from the trap center from motor movement. In order to see how velocity correlates with different forces, traces were analyzed over 5 s windows to find the average force, or bead position relative to the trap center. The average velocity that correlates with each window was then calculated using a linear fit. These datasets were then used to construct a force-velocity curve.

### Stochastic Simulation

In our computational model, a motor protein contains three elements: motor head, stalk, and non-motor tail. Motor head is a stochastic stepper following the three-state force-velocity relation (Equations 1 and 2). Parameters for the three-state model were taken from experimental data for Kif15 (Table 1). At each time step, forward stepping occurs with probability  $v(F)dt$ , where  $v(F)$  is the force-dependent speed of the motor, and  $dt$  is the time increment per integration step. Under resisting load, a backward step occurs with rate  $k_b e^{f/\delta_b}$ , where  $k_b = 0.25/s$  is the unloaded backward stepping rate,  $f$  is the magnitude of the resisting load, and  $\delta_b = 4$  nm is the force sensitivity of the backward steps. Values of  $k_b$  and  $\delta_b$  were chosen so that backstepping occurs about 30% of stepping events, as measured experimentally. Unbinding of a motor head occurs with rate  $(1/2)k_m^{off} [1 + \text{erf}(\{f - f_{stall}\}/2\sigma_s)]$ . Here,  $k_m^{off} = 1/s$  is the basal off rate,  $\text{erf}(x)$  is the error function,  $f$  is the magnitude of the resisting load,  $f_{stall} = 2.7$  pN is the stall force, and  $\sigma_s = 0.01$  pN is the transition width of the error function. An unbound motor head immediately relaxes to its equilibrium position and rebinds to the microtubule with rate 5/s.

For the tail domain, an unbinding event follows a form similar to unbinding of the motor head:  $(1/2)k_t^{off} [1 + \text{erf}(\{f - f_t\}/2\sigma_t)]$ , with  $k_t^{off} = 10/s$ ,  $f_t = 6.1$  pN (rupture force of Coil-1), and  $\sigma_t = 0.5$  pN. An unbound tail domain immediately relaxes to its equilibrium position and rebinds to the microtubule. The stalk is modeled as a Hookean spring of stiffness 0.5 pN/nm, and force on the motor increases linearly with the distance between its motor head and tail. Choice of model parameters whose values are not experimentally available were made to approximately reproduce the experimental observations in other aspects, such as the motor head stalling and tail rupturing. For the purpose of examining dependence on different model components, in particular, backstepping and tethering (Figure 5D–5G), precise values of model parameters are not important.

A microtubule was considered to be rigidly linked to a trapped bead of stiffness 0.04 pN/nm, the same as in the experiment. Time evolution of its position was made via Brownian dynamics method, with a stochastic velocity Verlet integration algorithm. Each run started with five motors. Their motor heads are initially bound to the microtubule and tails are bound to the substrate. After the simulation starts, motors walk along the microtubule and slide it. The microtubule's position and force were recorded in time. In simulations with tethers (Figures 5F and 5G), five additional motors were introduced, with their tail domains bound to the cargo microtubule, while their motor domains were affixed to the substrate. For these tethers, rupturing of the tails from the cargo microtubule can happen, but their motor domains are immobile, which mimic the situation that can occur during microtubule gliding (Figure 5A), or in an anti-parallel microtubule bundle where motor heads are in rigor states. A more extensive analysis of this model will be published elsewhere.

## QUANTIFICATION AND STATISTICAL ANALYSIS

All experiments were repeated until convergence and high N to ensure that the data were robust. Average and standard deviation are reported throughout the paper and figure legends. Error bars are standard error. The N value for each experiment is reported in each figure. N represents: number of stalls (Figures 1C and 2C), number of steps (Figures 1D and 2D), number of dwells (Figures 1E and 2E), number of velocity traces (Figure 1F), number of processivity measurements (Figure 1G), number of lifetime measurements (Figures 3B and 3E), number of rupture events (Figures 3C and 3F), number of parallel bundle measurements (Figure 4C), number of anti-parallel bundle measurements (Figure 4D), and number of gliding traces (Figure 5). In the custom written algorithms used for analysis, a sliding Student's t test was used to determine boundaries (steps, dwells, stalls, change in direction) in each trace.